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**ITU-T**

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**J.23**

**TELEVISION AND SOUND TRANSMISSION**

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**PERFORMANCE CHARACTERISTICS OF  
7 kHz TYPE (NARROW BANDWIDTH)  
SOUND - PROGRAMME CIRCUITS**

**ITU-T Recommendation J.23**

(Extract from the *Blue Book*)

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## NOTES

1 ITU-T Recommendation J.23 was published in Fascicle III.6 of the *Blue Book*. This file is an extract from the *Blue Book*. While the presentation and layout of the text might be slightly different from the *Blue Book* version, the contents of the file are identical to the *Blue Book* version and copyright conditions remain unchanged (see below).

2 In this Recommendation, the expression “Administration” is used for conciseness to indicate both a telecommunication administration and a recognized operating agency.

## Recommendation J.23

### PERFORMANCE CHARACTERISTICS OF 7 kHz TYPE (NARROW-BANDWIDTH) SOUND-PROGRAMME CIRCUITS<sup>1), 2), 3), 4)</sup>

#### Circuits of medium quality for monophonic transmission

(amended at Geneva, 1980 and at Melbourne, 1988)

The CCITT,

*considering*

- (a) that it is necessary to set transmission standards for sound-programme circuits;
- (b) that quality requirements for the hypothetical reference circuit are established for analogue sound programmes;
- (c) that advantage should be taken of the technical evolution made possible by the introduction of digital techniques, particularly for mixed analogue and digital circuits,

*recommends*

that, with due regard to the application constraints, equipment for new circuits shall meet the requirements laid out below.

#### 1 Application

The Recommendation applies to homogeneous analogue or mixed analogue-and-digital circuits.

The requirements below apply to the hypothetical reference circuit (HRC) defined in Recommendation J.11.

For estimation of the performance of circuits shorter or longer than the HRC, see CCIR Recommendation 605.

*Note 1* – For all-digital circuits a separate Recommendation might be envisaged after further study.

*Note 2* – For further work, CCIR Report 496 may be consulted. This Report also draws attention to certain differences between CCIR and OIRT Recommendations.

#### 2 Interface characteristics

##### 2.1 Test conditions

When circuit performance is to be measured, the system output shall be terminated by a balanced test load, nominally 600  $\Omega$  resistive.

##### 2.2 Impedance

System input impedance	600 $\Omega$ , balanced <sup>5)</sup>
System output impedance, provisionally	Low, balanced

<sup>1)</sup> This Recommendation corresponds to CCIR Recommendation 503. CCIR has agreed, at its XVIth Plenary Assembly, Dubrovnik, 1986, that CCIR Recommendation 504-2 will not be published in the next CCIR book.

<sup>2)</sup> For the definition of absolute power, relative power and noise levels, see CCIR Recommendation 574.

<sup>3)</sup> Sound-programme circuits of the 5 kHz type are widely used in North America.

<sup>4)</sup> 6.4 khz-type narrow bandwidth sound-programme circuits are still being used in some countries.

<sup>5)</sup> The tolerance, permitted reactance and degree of unbalance need further study.

The open-circuit output level shall not decrease more than 0.3 dB within the nominal frequency range, if the output is terminated by the specified test load.

The reactive part of the source impedance must be restricted to 100 Ω max. (provisional value) within the nominal frequency range.

2.3 *Levels*

Input maximum programme level	+ 9 dBm0s
Insertion gain (1 kHz at – 12 dBm0)	0 dB
Adjustment error, within	± 0.5 dB
Variation over 24 hours not to exceed	± 0.5 dB
Relative level (see Recommendation J.14)	+ 6 dBrs

If the broadcast organizations wish to have closer tolerances, it is necessary for the receiving broadcasting organizations to insert additional trimming attenuators.

3 **Overall performance**

3.1 *Common parameters*

3.1.1 *Gain/frequency response*

Reference frequency	1 kHz (nominal value)
The response shall be measured at	– 12 dBm0s

The gain/frequency response is given in Table 1 /J.23.

If broadcasting organizations wish to have closer tolerances, it is necessary for the receiving broadcasting organization to insert additional equalizers.

TABLE 1/J.23

Frequency (kHz)	Response (dB)
$0.05 \leq f < 0.1$	+ 1 to – 3
$0.1 \leq f \leq 6.4$	+ 1 to – 1
$6.4 < f \leq 7$	+ 1 to – 3

3.1.2 *Group delay variation*

Difference  $\Delta\tau$ , between the value of group delay at certain frequencies and the minimum value is given in Table 2/J.23. Between the points defined in Table 2/J.23, the tolerance limit varies linearly in a linear-delay/logarithmic-frequency diagram.

TABLE 2/J.23

Frequency (kHz)	$\Delta\tau$ (ms)
0.05	80
0.1	20
6.4	5
7	10

### 3.1.3 Noise

The measurement is to be made with an instrument conforming to CCIR Recommendation 468.

For radio-relay systems the requirements of Table 3/J.23 shall be met for at least 80% of the total time of any 30-day period. For 1% of the time an additional impairment of 4 dB, and for 0.1% of the time an additional impairment of 12 dB is acceptable.

TABLE 3/J.23

Noise	Transmission system	
	Analogue	Digital (3 codecs cascaded)
Idle channel noise, max (dBq0ps)	- 44	- 49
Programme-modulated noise, max (dBq0ps)	- 32	- 37

Programme-modulated noise can only occur on sound-programme circuits which are equipped with companders (for example types of circuits corresponding to Recommendation J.31).

This noise value may be measured with the aid of an auxiliary sinusoidal test signal + 9 dBm0s/60 Hz which has to be suppressed by a high-pass filter ( $f_0 \leq 400$  Hz,  $a \geq 60$  dB/60 Hz) before the measuring set.

CCIR Report 493 indicates that if a compandor is used, an improved signal-to-noise is necessary to avoid objectionable effects with some programme material.<sup>6)</sup>

*Note* – For digital systems appropriate values are under study. For further information see CCIR Report 647.

### 3.1.4 Single tone interference

Level of any individual tone:

$$\leq (-73 + \psi) \text{ dBm0s}$$

where  $\psi$  is the weighting factor (positive or negative) as per CCIR Recommendation 468 at the particular frequency.

<sup>6)</sup> Administrations are urged to supply additional information on an appropriate value.

For sound-programme transmissions over carrier systems, occurrence of carrier leaks can be expected. For this reason, stop filters may be provided in the carrier frequency path which can be switched in, if required, to suppress the tones otherwise audible in the upper frequency range from 8 to 15 kHz. For a hypothetical reference circuit, a 3 dB bandwidth of less than 3% for stop filters, referred to the mid-frequency, is recommended. The use of stop filters influencing frequencies below 8 kHz should be avoided.

### 3.1.5 *Disturbing modulation by power supply*

The level of the strongest unwanted side component due to modulation caused by low-order interference components from 50 Hz or 60 Hz mains shall be less than – 45 dBm0s with a test signal of 1 kHz at alignment level 0 dBm0s.

### 3.1.6 *Non-linear distortion*

#### 3.1.6.1 *Harmonic distortion*

The total harmonic distortion (THD) shall be measured with the input signal at + 9 dBm0s.

The duration for which a single-tone is to be transmitted at this level should be restricted in accordance with Recommendations N.21 and N.23.

The THD when measured with a true-RMS meter shall not be less than the following requirements shown in Table 4/J.23.

TABLE 4/J.23

Input frequency (kHz)	Total harmonic distortion
$0.05 \leq f < 0.1$	2% (-25 dBm0s)
$0.1 \leq f \leq 2.0$	1.4% (-28 dBm0s)

*Note* – If THD cannot be measured directly, compliance is considered to be fulfilled if the second or third harmonics are measured selectively and a calculated value of  $k$  meets the requirement:

$$k = \sqrt{k_2^2 + k_3^2}$$

where  $k_2$  is the second harmonic coefficient and  $k_3$  is the third harmonic coefficient.

#### 3.1.6.2 *Intermodulation*

With input signals of 0.8 kHz and 1.42 kHz, each at a level of + 3 dBm0s, the third order difference tone at 0.18 kHz shall be less than 1.4% (- 34 dBm0s).

#### 3.1.6.3 *Distortion products measured by shaped noise*

Under study. See CCIR Report 640 (Kyoto 1978).

### 3.1.7 *Error in reconstituted frequency* (applies only to FDM systems)

Not to be greater than 1 Hz.

*Note* – A maximum error of 1 Hz is in principle acceptable where there is only a single transmission path between the signal source and the listener.

Where the broadcast network can involve two or more parallel paths, e.g. commentary and separate sound channels, or radio broadcast from different transmitters on the same frequency, unacceptable beats may occur unless zero error can be assured. The CCITT is studying methods of effecting this in all recommended systems.

### 3.1.8 *Intelligible cross-talk ratio*

3.1.8.1 The intelligible near-end and far-end cross-talk ratios between sound-programme circuits, or from a telephone circuit (disturbing) into a sound-programme circuit (disturbed) shall be measured selectively in the disturbed circuit at the same frequencies as those of the sinusoidal test signal applied to the disturbing circuit, and shall not be less than the values of Table 5/J.23.

TABLE 5/J.23

Frequency (kHz)	Crosstalk attenuation (dB)
$f < 0.5$	Slope 6 dB/octave
$0.5 \leq f \leq 3.2$	74
$f > 3.2$	Slope - 6 dB/octave

3.1.8.2 The near-end and far-end cross-talk attenuations between a sound-programme circuit (disturbing circuit) and a telephone circuit (disturbed circuit) shall be at least 65 dB.

*Note 1* – It is understood that this value is defined between the relative levels applicable to telephone circuits. (Administrations are invited to submit contributions on methods for measuring this parameter.)

*Note 2* – The attention of Administrations is drawn to the fact that it is in some cases difficult or impossible to meet these limits. This may occur when unscreened pairs are used for a long audio-frequency circuit (e.g. about 1000 km or longer), or in certain carrier systems on symmetric pair cables, or at low frequencies (e.g. below about 100 kHz) on certain coaxial cable carrier systems. If sub-standard performance is to be avoided, such systems or parts of systems must not be used for setting up programme channels.

*Note 3* – When 4000 pW0p or more noise is continuously present in the telephone channel (this may be the case in satellite systems, for example), a reduced cross-talk ratio of 58 dB between a sound-programme circuit and a telephone circuit is acceptable.

*Note 4* – The attention of Administrations is drawn to the fact that, because of cross-talk which may occur in terminal modulating and line equipment, special precautions may have to be taken to meet the above cross-talk limits between two sound-programme circuits, simultaneously occupying the go and return channels respectively, of a carrier system (the most economical arrangement) because in those circumstances they occupy the same position in the line-frequency band (see Recommendation J.18).

*Note 5* – The value indicated is based on the assumption that sine wave test signals are used. The use of the test signal as described in Recommendation J.19 is under study.

*Note 6* – The effect of cross-talk from a sound-programme circuit into a telephone circuit is not a question of secrecy, but rather of subjective disturbance by an interfering signal whose character is noticeably different from random noise or babble.

The frequency offset adopted for some sound-programme equipment allows a reduction of cross-talk from a telephone circuit into a sound-programme circuit. However, in the reverse direction, this reduction of cross-talk remains only for speech material but is practically ineffective for music material.

### 3.1.9 *Amplitude linearity*

When a 1 kHz input signal is stepped from - 6 dBm0s to + 6 dBm0s, or vice versa, the output level shall change accordingly by  $12 \pm 0.5$  dB.

### 3.2 *Additional parameters for stereophonic programme transmission*

Not applicable, this section concerns 15 kHz type sound-programme circuits (see Recommendation T.21).

3.3 *Additional requirements for digital systems*

3.3.1 If a test signal is harmonically related to the sampling frequency, measuring difficulties may arise. In this case the nominal 1 kHz test signal must be offset. The Recommendation O.33 recommends 1020 Hz.

3.3.2 *Unbalance of the limitation level*

The difference between those levels which lead to a limitation of the positive or negative half-wave of the test signal shall not exceed 1 dB.

3.3.3 *Intermodulation with the sampling signal*

Intermodulation products ( $f_d$ ) caused by non-linearities may occur in the sound-channel when the sampling signal ( $f_o$ ) is combined with the inband audio signals ( $f_i$ ) or out-of-band interfering signals ( $f_a$ ).

3.3.3.1 *Inband intermodulation*

The following combination rule applies:  $f_d = f_o - nf_i$ .

Only values with  $n = 2$  or 3 are of importance.

The level difference between a 0 dBm0s signal ( $f_i$ ) and the intermodulation products ( $f_d$ ) shall not be less than 40 dB.

A restriction to the  $f_i / f_d$  values in Table 6/J.23 is sufficient.

TABLE 6/J.23

	$n = 2$		$n = 3$	
$f_i$ (kHz)	5	7	3	5
$f_d$ (kHz)	6	2	7	1

3.3.3.2 *Out-of-band intermodulation*

The following combination rule applies:  $f_d = nf_o \pm f_a$ .

Only values with  $n = 1$  or 2 are of importance.

The level difference between a 0 dBm0s signal ( $f_a$ ) and the intermodulation products ( $f_d$ ) shall not be less than 60 dB.

A restriction to the  $f_a / f_d$  values in Table 7/J.23 is sufficient.

TABLE 7/J.23

	$n = 1$		$n = 2$	
$f_a$ (kHz)	15	17	31	33
$f_d$ (kHz)	1			



### 3.3.4 *Further parameters*

Characteristics for bit errors, clicks, jitters, etc., are under study. (See Study Programme 18A/CMTT and CCIR Report 647.)

#### **Bibliography**

CCIR Document [1978-1982]: CMTT/68 (OIRT).